Keelboat Sailing Instruction to CYA standards

Wavelength

Tides

When Sailing in tidal waters you need to know the tidal height and how it will change with time for example when you anchor, transit a region of shallow water or dock. In the Basic course you learned how to read a Tide Table for example the one for St. John on the last page of this document. Let's suppose you plan to anchor near St John. You plan to arrive on June 6 2010 at 1400 Daylight Savings Time and the charted water depth in the anchorage is 7 ft. Since the tide tables are in standard time the planned time of arrival is 1300 standard time. Looking at the table there is a low tide near this time at 1248 of 6.6 ft so the anticipated depth is: 7ft (charted depth) + 6.6 ft (tidal height) = 13.6 ft or nearly 14 ft. Let's say you plan to stay there until the next morning at 0900 So during this time period the tidal heights are a minimum of 6.6 feet and a maximum of 26.6 feet. So the depth in that anchorage will vary between 13.6 ft and 33.6 ft (26.6ft + 7 ft). So no issue with grounding but you should plan for a scope appropriate to 34 feet of water for the overnight stay. When you arrive at the anchorage you should check the depth to see that it is close to the anticipated 14 feet.

Let's suppose however that you now are delayed and arrive at 1600 DST, (1500 PST) now what is the predicted depth? 1500 is between the times of low and high tide. There are various ways of calculating intermediate tidal heights however one of the simplest is the "Rule of Twelves". This says that the tidal height changes according to the following.

First we calculate the tidal range or difference in height between adjacent high and low tides which span the time range of interest. If we call this R then

1 hour after high (or low tide) the height has changed by $1/12 \ge R$ 1 hour later it has changed by a further $2/12 \ge R$ 1 hour later it has changed by a further $3/12 \ge R$ 1 hour later it has changed by a further $3/12 \ge R$ Keelboat Sailing Instruction to CYA standards

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1hour later it has changed by a further $2/12 \ge R$ 1 hour later it has changed by a further $1/12 \ge R$ Since diurnal tides are a little less than 6 hours apart this spans the period between adjacent high and low tides or vice versa.

So we can tabulate this as below

Time after high or low	Total Change in depth
tide	
1 hour	+/- R/12
2 Hour	+/- 3R/12
3 Hour	+/- 6R/12
4 Hour	+/- 9R/12
5 hour	+/- 11R/12
6 Hour	+/- 12R/12 (+/- R)

Where + values are used if the tide is rising (i.e. Starting from low tide) and – values if it is falling (i.e. starting from high tide)

So using the example above 1500 PST is approximately 2 hours after the low tide at 1248 and the range R is 22.6-6.6 t or 16 ft. From the formula above the tide will have risen by $+3 \times 16/12$ or 4ft. So the tidal height will be 6.6 +4 ft. or 10.6 ft. so we now would expect to anchor in

7ft. (charted depth) + 10.6 ft. (tidal height) = 17.6 ft. or nearly 18 ft.

So when we arrive the water depth on our depthsounder should correspond to 18 ft.

Adapted from a Coastal Navigation Course by Jamie Gordon

TABLE DES MARÉES April-avril										20)10)		SAINT JOHN							HN	A Z+4	
								May-mai											June-juin				
Day	Time	Feet	Metres	jou	heure	pieds	mètres	Day	/ Time	Feet	Metres	-		17	mètres	Day	/ Time	Feet	Metres	jour	heure	pieds	mètres
	0048 0707 1315 1927	27.6 1.0 26.2 2.3	8.4 0.3 8.0 0.7	FR	0026 0644 1251 1859	3.0	7.8 0.9 7.4 1.3	SA	1342 1952	26.6 2.3 24.6 4.3	8.1 0.7 7.5 1.3	SU	0043 0704 1312 1922	24.6	0.7	TU	0222 0843 1452 2102	4.3 23.6		WE	0204 0827 1437 2051	27.2 1.6 25.9 3.0	0.5
	0135 0755 1404 2015	26.9 1.6 25.3 3.3	8.2 0.5 7.7 1.0	SA	0104 0723 1330 1940	3.0 24.3	7.8 0.9 7.4 1.3	SU	0159 0820 1430 2040	25.9 3.3 24.0 4.9	7.9 1.0 7.3 1.5	MO	0128 0751 1359 2011	- 2.0	0.8	WE	0309 0929 1539 2150	23.3	7.4 1.5 7.1 2.0		0258 0921 1532 2147	26.6 2.0 25.6 3.3	8.1 0.6 7.8 1.0
3 SA SA	0224 0844 1455 2106	26.2 3.0 24.3 4.6	8.0 0.9 7.4 1.4	SU	0145 0806 1413 2025	25.3 3.3 24.0 4.6	7.7 1.0 7.3 1.4	мо	0248 0910 1521 2131	24.9 4.3 23.3 5.9	7.6 1.3 7.1 1.8		0218 0841 1451 2104	25.9 2.6 24.6 4.3		TH	0358 1016 1628 2240	5.0	7.2 1.7 7.0 2.1		0356 1017 1629 2247	25.9 2.6 25.6 3.6	7.9 0.8 7.8 1.1
	0315 0937 1548 2159	24.9 3.9 23.3 5.6	7.6 1.2 7.1 1.7		0231 0854 1502 2116	25.3 3.6 23.6 5.2	7.7 1.1 7.2 1.6		0340 1002 1614 2226	24.0 4.9 22.6 6.6	7.3 1.5 6.9 2.0		0312 0936 1547 2202	25.6 3.0 24.3 4.6		FR	0449 1105 1719 2333	22.6 6.2 22.6 7.2	6.9 1.9 6.9 2.2	SA	0456 1116 1730 2349	25.3 3.3 25.3 3.6	7.7 1.0 7.7 1.1
	0410 1033 1646 2258	24.0 4.9 22.3 6.6	7.3 1.5 6.8 2.0		0323 0948 1558 2213	24.6 3.9 23.3 5.6	7.5 1.2 7.1 1.7	WE	0435 1057 1710 2323	23.3 5.9 22.3 7.2	7.1 1.8 6.8 2.2		0411 1035 1647 2304	25.3 3.3 24.3 4.6	7.7 1.0 7.4 1.4		0542 1156 1810	0.0	6.8 2.0 6.9	20 SU DI	0600 1216 1831	24.6 3.6 25.3	7.5 1.1 7.7
U	0510 1134 1748	23.3 5.9 22.0	7.1 1.8 6.7	21 WE ME	0422 1048 1700 2317	24.6 4.3 23.3 5.6	7.5 1.3 7.1 1.7		0534 1153 1808	22.6 6.2 22.0	6.9 1.9 6.7	21 FR VE	0514 1136 1750	3.6	7.6 1.1 7.5	SU	0026 0636 1248 1901	6.9 22.0 6.6 22.6	2.1 6.7 2.0 6.9		0053 0704 1318 1932	3.6 24.3 4.3 25.3	1.1 7.4 1.3 7.7
WE	0001 0614 1236 1851	7.2 22.6 6.2 21.7	2.2 6.9 1.9 6.6	22 TH JE	0527 1153 1807	24.3 4.3 23.6	7.4 1.3 7.2	FR	0022 0633 1250 1904	7.2 22.3 6.6 22.3	2.2 6.8 2.0 6.8	SA	0009 0619 1239 1853	4.3 24.6 3.6 24.9	1.3 7.5 1.1 7.6	мо	0119 0729 1338 1950	6.6 22.0 6.6 23.0	2.0 6.7 2.0 7.0		0155 0807 1418 2031	3.6 24.0 4.6 25.3	1.1 7.3 1.4 7.7
TH	0104 0716 1337 1950	7.2 22.6 6.2 22.0	2.2 6.9 1.9 6.7	FR	0023 0635 1259 1912	4.9 24.6 3.9 24.3	1.5 7.5 1.2 7.4	SA	0119 0729 1343 1956	7.2 22.3 6.2 22.6	2.2 6.8 1.9 6.9	SU	0113 0724 1340 1953	3.6 24.6 3.6 25.6	1.1 7.5 1.1 7.8	TU	0209 0819 1427 2037	5.9 22.0 6.2 23.6	1.8 6.7 1.9 7.2	WE	0254 0906 1515 2126	3.3 24.0 4.6 25.6	1.0 7.3 1.4 7.8
FR	0204 0814 1431 2043	6.9 22.6 5.9 22.6	2.1 6.9 1.8 6.9	SA	0130 0741 1401 2014	4.3 24.9 3.3 25.3	1.3 7.6 1.0 7.7	SU	0211 0821 1432 2042	6.6 22.3 5.9 23.0	2.0 6.8 1.8 7.0	MO	0214 0825 1438 2050	3.3 24.9 3.6 25.9	1.0 7.6 1.1 7.9	WE	0257 0907 1513 2123	5.2 22.6 5.6 24.3	1.6 6.9 1.7 7.4		0349 1000 1608 2218	3.3 24.0 4.6 25.6	1.0 7.3 1.4 7.8
SA	1519	6.2 23.0 5.6 23.0	1.9 7.0 1.7 7.0	SU	0232 0842 1459 2110	3.3 25.6 2.6 26.2	1.0 7.8 0.8 8.0	MO	0258 0908 1516 2124	5.6 22.6 5.6 23.6	1.7 6.9 1.7 7.2	TU	0312 0922 1533 2143	2.6 24.9 3.3 26.6	0.8 7.6 1.0 8.1	TH	0343 0953 1559 2207	4.3 23.3 5.2 25.3	1.3 7.1 1.6 7.7	FR	0439 1050 1658 2306	3.0 24.3 4.6 25.9	0.9 7.4 1.4 7.9
SU		5.6 23.6 4.9 23.6	1.7 7.2 1.5 7.2	MO	0329 0939 1552 2203	2.3 25.9 2.3 26.9	0.7 7.9 0.7 8.2		0341 0950 1557 2204	4.9 23.3 5.2 24.3	1.5 7.1 1.6 7.4		0405 1015 1624 2234	2.3 24.9 3.3 26.6	0.7 7.6 1.0 8.1	FR	0428 1038 1644 2252	3.3 24.0 4.6 25.9	1.0 7.3 1.4 7.9	SA	0527 1136 1744 2351	3.0 24.3 4.6 25.9	0.9 7.4 1.4 7.9
	1029 1638	4.9 24.0 4.6 24.3	1.5 7.3 1.4 7.4	TU	0422 1031 1643 2252	1.3 26.2 2.0 27.2		WE	0421 1030 1636 2242	3.9 23.6 4.6 24.9	1.2 7.2 1.4 7.6	TH	0455 1105 1713 2321	2.0 24.9 3.6 26.6	0.6 7.6 1.1 8.1	SA	0514 1123 1730 2338	2.6 24.6 3.9 26.6	0.8 7.5 1.2 8.1			3.3 24.3 4.6	1.0 7.4 1.4
13 TU MA	1713	3.9 24.3 4.3 24.9	1.2 7.4 1.3 7.6	WE	0512 1121 1731 2339	1.0 26.2 2.3 27.2	0.3 8.0 0.7 8.3	TH	1715	3.3 24.0 4.3 25.6	1.0 7.3 1.3 7.8		0542 1152 1800	2.0 24.9 3.9	0.6 7.6 1.2		0559 1208 1817	2.0 24.9 3.3	0.6 7.6 1.0		0034 0653 1301 1910	25.6 3.3 24.3 4.9	7.8 1.0 7.4 1.5
14 WE ME	1747	3.6 24.3 4.3 25.3	1.1 7.4 1.3 7.7		0559 1209 1818	1.3 25.9 2.6	0.4 7.9 0.8		0539 1148 1755	2.6 24.3 3.9	0.8 7.4 1.2	SA	0628	26.2 2.3 24.6 4.3	8.0 0.7 7.5 1.3	14 мо LU		26.9 1.6 25.6 3.0	8.2 0.5 7.8 0.9		1342	25.3 3.6 24.3 5.2	7.7 1.1 7.4 1.6
15 TH JE	1213 .	3.0 24.3 3.9	0.9 7.4 1.2	FR	0026 0646 1255 1905	26.9 1.6 25.3 3.3	8.2 0.5 7.7 1.0	SA	0620	25.9 2.3 24.6 3.9	7.9 0.7 7.5 1.2	SU	0713	25.9 3.0 24.3 4.6	7.9 0.9 7.4 1.4	15 TU MA	1345	27.2 1.3 25.9 3.0			1422	24.9 4.3 24.0 5.6	7.6 1.3 7.3 1.7
												МО	0758	25.6 3.6 24.0 5.2	7.8 1.1 7.3 1.6								